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=> s tungsten leach? and reduc? and oxid?
       204929 TUNGSTEN
       122287 LEACH?
           81 TUNGSTEN LEACH?
                 (TUNGSTEN(W)LEACH?)
      2365089 REDUC?
      3206799 OXID?
L1
            2 TUNGSTEN LEACH? AND REDUC? AND OXID?
=> d 1-2 ibib abs hitstr
L1 ANSWER 1 OF 2 HCAPLUS COPYRIGHT 2008 ACS on STN
ACCESSION NUMBER:
                       1982:38798 HCAPLUS
DOCUMENT NUMBER:
                        96:38798
ORIGINAL REFERENCE NO.: 96:6393a,6396a
TITLE:
                        Partitioning molybdenum and tungsten from a mixed
                        calcium molybdate-calcium tungstate precipitate
                        Rappas, Alkis S.; Menashi, Jameel; Douglas, Donald A.
INVENTOR(S):
PATENT ASSIGNEE(S):
                        Cabot Corp., USA
                        U.S., 35 pp.
SOURCE:
                        CODEN: USXXAM
DOCUMENT TYPE:
                        Patent
LANGUAGE:
                        English
FAMILY ACC. NUM. COUNT: 1
PATENT INFORMATION:
    PATENT NO.
                       KIND
                              DATE
                                         APPLICATION NO.
                                                                 DATE
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US 4278644 A 19810714 US 1980-140436 19800415
PRIORITY APPLN. INFO::

AB Superalloy or tool steel scrap containing Cr, V, Mo, and W is calcined with Na2CO3 in air. Subsequent leaching produces the soluble Mo042-, V043-, W042-, and Cr042- for separation from the insol. oxides of base metals. The V, Mo, and W are separated from the leach solution, and Cr6+ is reduced to Cr3+. A mixed solution containing CaO.nv205, CaMo04, and CaW04 is produced, and is treated with: (a) carbonated water or formic acid, to dissolve V for recovery; and (b) H202-containing H2SO4, to precipitate CaSO4

for concentrating W and Mo. The W is precipitated by thermally decomposing the peroxy

complexes. No aqueous effluents are produced, and reagent consumption is decreased. Thus, the grindings of Ni-base superalloy [80329-36-8] (Ni 55, Co 2.5, Fe 5.5, Cr 15.5, No 16, W 3.8, and miscellaneous 1%) were mixed with

equal weight of Na2CO3, calcined in air 4 h at 1100°, and leached with water for extraction of Mo 96.3-9.2, W, and Cr 98.3-9.8%. Recovery was increased as the nominal particle size of the grindings decreased from 400 to 75 μ. The mixture of shredded turnings and grindings was also successfully calcined for leach extraction A synthetic leach solution containing the

Na salts of Cr6+ (47 g/L), Mo6+, W6+, and V5+ was reduced with HCO2Na [141-53-7] in the presence of CO2. The content of Cr6+ was thereby decreased to 2.5 g/L for the improved removal of Mo, W, and V. The CaCO3 in filter cake was selectively dissolved by formic acid [64-18-6], together with some CaCrO4, to decrease the precipitate amount for

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recovery of Mo and W. The CaMoO4 + CaWO4 filter cake was treated with H2SO4 containing NH4HSO4 and H2O2, the CaSO4 tailings were precipitated out, and the

solution was heated to precipitate the W values. Residual solution was treated with

activated charcoal to remove the residual W from O-rich solution

L1 ANSWER 2 OF 2 HCAPLUS COPYRIGHT 2008 ACS on STN

ACCESSION NUMBER: 1967:435019 HCAPLUS DOCUMENT NUMBER: 67:35019

DOCUMENT NUMBER: 67:35019

ORIGINAL REFERENCE NO.: 67:6631a,6634a

TITLE: Extractive separation of molybdenum and tungsten from

acid solutions

AUTHOR(S): Petrov, M. A.; Maslenitskii, N. N.; Davydova, A. D. SOURCE: Tsvetnye Metally (Moscow, Russian Federation) (1967),

40(3), 16-20

CODEN: TVMTAX; ISSN: 0372-2929
DOCUMENT TYPE: Journal

LANGUAGE: Journal Russian

AB Mo and WO3 were extracted from an impure H2O solution, containing Mo .apprx.5, WO3

.apprx.5, P. apprx.0.5, Ca .apprx.12, and $\mathrm{HGl}\ 15$ g./l., with a solution of tech. tertiary C7-9 aliphatic amines in an unstated organic solvent. The best amine concentration in the organic phase was 50 g./l. The best

organic:aqueous phase volume ratio was 1:3. Extraction after 3 stages was Mo 99.45 and MO3 99.85%. Increasing the HCl concentration >95 g./l. had little effect on the extraction of MO3.

decreased that of Mo to <50, and of P to <20%. Best HCl concentration was 5-15 g./l.; extraction of Mo and WO3 was almost complete and that of P was apparently dissolved in the form of heteropoly compds., since it was not extracted in the absence of the metals. Increasing

the HCl concentration to 73 g./l. increased the WO3/Mo partition coefficient to a maximum, which increased with increasing WO3/Mo ratio. Further acidity increase decreased the coefficient Increasing the aqueous:organic phase

volume ratio

(1-9) had little effect on the partition coefficient (74-80) at HCl 73 g./l.

and increased it (14-86) at HCl 150 g./l. A 1-stage separation was not feasible, since 30-60% of the Mo was extracted with the WO3. The organic olution

containing Mo 17.5 and WO3 16 g./l. was extracted with about the stoichiometric amount of NaOH in H2O solution; extraction was .apprx.99.9%. Increasing the NaOH

concentration (5-20 g./1.) decreased the number of extraction stages (6-3) and the NaOH $\,$

solution volume and increased the metal concentration in the extract The oxidized metal compds. were extracted before the reduced compds, and Fe hydroxide was precipitated The extract NaOH concentration could be

decreased to 2-4 g./l. without affecting the process.

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